## Investigation of the April 19, 2018, Communication Tower Collapse in Fordland, Missouri.

U.S. Department of Labor Occupational Safety and Health Administration Directorate of Construction

October 2018



### Report

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#### TABLE OF CONTENTS

Executive Summary	5
Introduction	7
Incident Description	10
Observations of Collapsed Tower	11
Structural Analysis and Discussion	14
Conclusion	19
Appendix A – Erection Drawings	20
Appendix B – Fabrication Drawings	34
Appendix C – Photographs (April 23, 2018)	50
Appendix D – Photographs (August 1, 2018)	58

#### **LIST OF FIGURES**

Figure 1. Project Location	5
Figure 2. Typical Bracing Elevation of Tower Legs	
Figure 3. Typical Tower Cross Section	8
Figure 4. Tower Elevation (TCI Structural Analysis Report Appendix E-1)	9
Figure 5. Collapsed Communication Tower (Google Image Search)	10
Figure 6 Top Section of Collapsed Communication Tower	11
Figure 7. Recovered Section of the Tower 90'–120'	12
Figure 8. Bent Tower Leg from the Recovered Section	12
Figure 9. Bent Redundant Member at 105' Tower Elevation	12
Figure 10. New bolts Installed on Two Diagonals at 100' Tower Elevation	12
Figure 11. Missing bolts at the 105' Tower Elevation	14
Figure 12. Representative Section from the Top of the Tower	15
Figure 13. Bolted Connection between Diagonals and Redundant Horizontal	15
Figure 14. TCI Diagonal Replacement (E-5)	17
Figure 15. Lemay Come-a-long Used On-site.	
Figure 16. T-532D Come-a-long in Debris	18
Figure 17. T-532D Come-a-long Salvage from Debris	18
Figure 18. TCI Temporary Frame Requirements (E-5)	19

#### **Executive Summary**

On April 19, 2018, an incident occurred in Fordland, Missouri where one employee was killed. The project involved the reinforcement of the KOZK 1,891-foot-tall guyed communication tower along Highway FF just north of Fordland, Missouri. The location of the tower is shown in Figure 1 (905 State Highway FF Fordland, MO 65602). The tower was initially designed and erected by Kline in 1971. Currently, Missouri State University (MSU) contracted Tower Consultants, Inc. (TCI) to design the required structural modifications necessary to support the transmission line replacement. TCI's scope of work involved creating construction documents, reviewing submittal drawings, observing the construction process including producing progress reports and assisting MSU in the bidding and contractor selection process. MSU selected Steve Lemay, LLC (Lemay) to serve as the contractor.

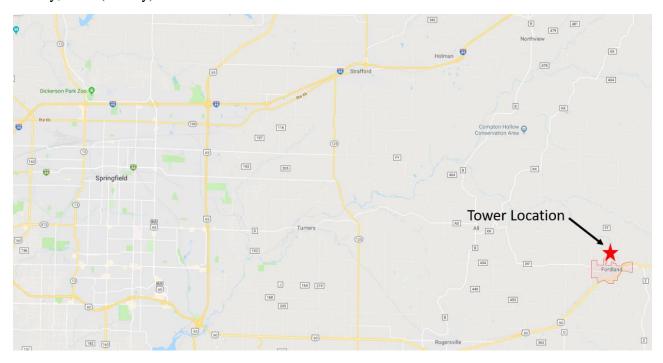


Figure 1. Project Location

The Occupational Safety and Health Administration's (OSHA) Regional Administrator, Region VII, asked the Directorate of Construction (DOC) in OSHA's National Office in Washington, D.C., to provide technical and engineering assistance to the OSHA Kansas City Area Office in its investigation of the tower collapse in Fordland, MO. At your request an engineer from DOC, Dr. Bryan Ewing, P.E., accompanied by Chester Ray, visited the incident site on April 23, 2018 and August 1, 2018. We also reviewed photographic evidence, witness interviews, construction documents, industry standards and engineering reports in preparation of this report. Attached is our report. After reviewing the documents and conducting independent structural analysis, we conclude the following:

1) TCI's suggested diagonal replacement procedure was flawed in that it compromised the effectiveness of the integrated surrounding braces and the load bearing capacity of the

- tower legs. A single diagonal brace could not be removed without affecting the integrity of the redundant brace because the braces share two common bolts at the diagonal/redundant connection.
- 2) The cause of the communication tower collapse was the weakening of the compressive strength of the tower legs by removing the bolts at the connection of the diagonals to the horizontal redundant. The compromised redundant effectively doubled the unbraced length of the tower leg which reduced the compressive capacity of the tower leg.
- 3) Lemay used an undersized come-a-long while removing the diagonal braces.
- 4) Lemay failed to provide the design of the required temporary frame for diagonal replacement above or below a guy level. TCI failed to confirm the use/design of a temporary frame as TCI is required to approve the adequacy of the temporary frame prior to diagonal replacement according to TCI's construction documentation.

#### **Introduction**

The 1,891-foot-tall guyed communication tower is constructed of 10-foot wide triangular sections. The legs of the tower consisted of 63 sections of solid round steel ranging in diameter from 4½" to 3¼" that were approximately 30 feet long. The lower 34 leg sections were constructed from high strength alloy steel with a design yield strength of 95 ksi. The design yield strength of the remaining leg sections was 47 ksi. The legs are connected by numerous angle struts, solid rod diagonals and horizontal redundants as shown in Figure 2. Although Figure 2 only shows one side, all three sides of the tower are similar. The angle struts consisted of double back-to-back A36 grade steel angles. The sizes of the angles vary and were either L3x2x<sup>1</sup>/<sub>4</sub> or L2<sup>1</sup>/<sub>2</sub>x2x<sup>1</sup>/<sub>4</sub>. The solid rod diagonals were fabricated from A36 grade steel and vary in diameter from 3/4" to 11/4". The horizontal redundants were 13/4" diameter solid A36 steel rods. The horizontal redundants were narrowed at its mid-span to accommodate the splice plates of the crossing diagonals. Both diagonals and the redundant were secured to each other with two through bolts. Note that Figure 2 shows the recommended split pipe reinforcement of the tower legs, but these split pipe reinforcements were not in place at the time of the incident. The 30-foot tower leg sections were field spliced together with six A325 bolts through factory fabricated flange plates at each end of the leg. The tower was stabilized by nine levels of guy wires. Each level had three guy lines (1 for each of the principal triangular directions of the tower). The diameter of the guy lines varied from 1-1/16" to 1-9/16" with a range of initial tensile forces between  $\pm 15$  kips to  $\pm 33$  kips depending on the temperature. A typical cross section of the tower and tower elevation are shown in Figures 3 and 4, respectively.

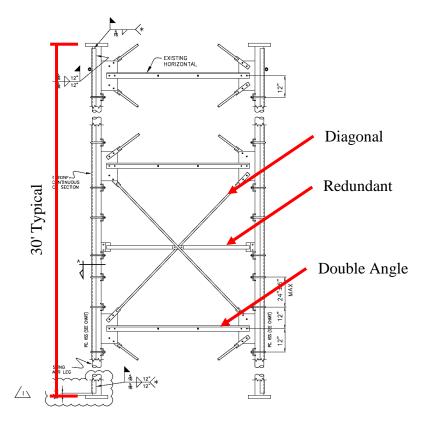


Figure 2. Typical Bracing Elevation of Tower Legs

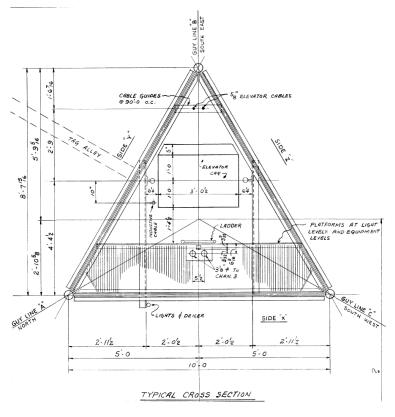


Figure 3. Typical Tower Cross Section

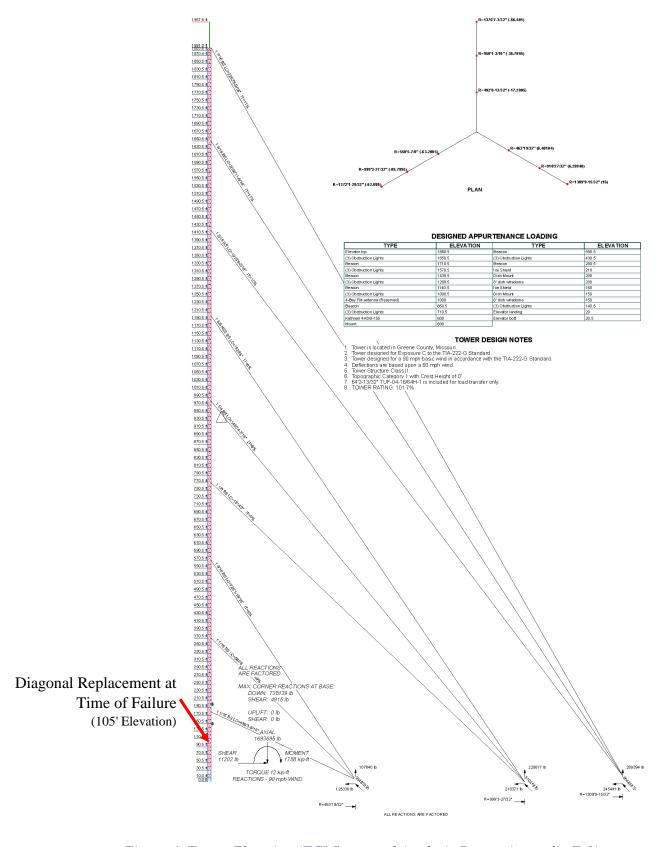


Figure 4. Tower Elevation (TCI Structural Analysis Report Appendix E-1)

TCI's May 19, 2017 structural analysis of the communication tower concluded that structural modifications were necessary for the tower to comply with the wind and ice loading requirements of ANSI/TIA-222-G. TCI recommended to replace one level of guy wires, reinforce 34 tower leg sections, replace 25 bays of diagonals and reinforce one level of horizontal struts. Lemay was contracted to perform the recommended structural modifications.

#### **Incident Description**

On April 19, 2018 at 9:33 AM, according to security camera surveillance footage, the KOZK communication tower collapsed resulting in the fatality of one worker and non-life-threatening injuries to four others. Lemay was performing structural modifications to the tower at the time of the collapse. An image of the resulting debris is shown in Figure 5. The contractor was replacing diagonals at the 105-foot level of the 1891-foot tall communication tower when the tower started to collapse. According to witness statements, the foreman of the five-man crew instructed the other employees on the tower to descend when audible structural distresses indicated the loss of structural integrity of the tower. The other employees on the tower managed to reach the ground and retreat from the falling debris. The foreman, however, decided to remain on the tower to discern and rectify the cause of the audible structural distresses and was struck and killed by the falling structure.



Figure 5. Collapsed Communication Tower (Google Image Search)



Figure 6 Top Section of Collapsed Communication Tower

Lemay arrived on-site on Monday, April 16, 2018 to begin working on the structural modifications to the communication tower the next day. The first two days involved preparation of the materials and tools and laying down and painting diagonals. Work on the tower was originally going to take place on Wednesday, but high winds caused the crew to delay work on the tower for another day. The crew began replacing diagonals on Thursday, April 19, 2018. They began replacing the diagonals at the 105' elevation. According to witness statements, the six replacement diagonals, the necessary equipment and the foreman were raised in a man-basket. One employee remained on the ground and the remaining employees went to assist with the replacement of diagonals. Two of the diagonals did not fit and were returned to the staging area on the ground so that the bolt holes could be bored out to facilitate their installation. The crew completed the diagonal replacement on two of the three sides and started work on the third. Witnesses stated they began hearing unusual sounds above them and the foreman instructed the other crew members to descend the tower as quickly as possible. The crew members made it off the tower before the collapse. However, the foreman did not, resulting in the lone fatality of the incident.

#### **Observations of Collapsed Tower**

As shown in Figure 5, it appears that as the tower began to collapse onto itself, the tower initially fell in the southern direction. Then the tower tilted and fell over itself back in a northern direction. As the top tiers of the tower fell, they remained essentially intact. As shown in Figure

6, all the guy wires disengaged from their anchor points and whipped about slashing through tree limbs and fencing. The man-basket, original and new diagonals and tools, including two comealongs were buried under the wreckage. The tower section from 90' to 120' was recovered and stored on-site for further observation. This tower section is shown in Figures 7 to 10. The slings and diagonals were found at the 105' tower elevation as shown in Figure 11. Several wires of the sling used for the come-a-long attachment to the tower panel point was severed and others were bird-nesting. A total of six bolted connections were missing. Two bolts were missing at the connection point between the two diagonals and the redundant horizontal bar. Two more bolts were missing from each gusset plate at the connection between the tower legs at the 100' elevation of the diagonals (see Figure 11). This was consistent with witness statements that the crew was working on the final third bay of diagonals at the 105' elevation at the time of the incident. The redundant bar and the tower leg appeared to have buckled.



Figure 7. Recovered Section of the Tower 90'–120'



Figure 8. Bent Tower Leg from the Recovered Section



Figure 9. Bent Redundant Member at 105' Tower Elevation



Figure 10. New bolts Installed on Two Diagonals at 100' Tower Elevation

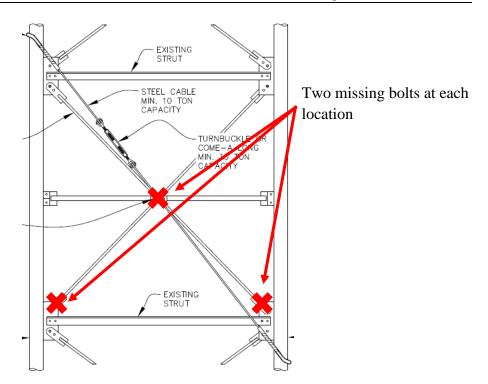


Figure 11. Missing bolts at the 105' Tower Elevation

#### **Structural Analysis and Discussion**

A guyed communication tower is a slender structure that relies on the guy wires to minimize flexural stresses generated by lateral loads, including wind, earthquake, etc. The tensioned guy wires were attached to the structure at various locations along the height of the tower. The compressive gravity loads, arising from its own weight, weight of the antennas and other equipment and resultant vertical loads of the guy wires, are supported by the axial strength of the tower. One of the characteristics of a structural member that affects its compressive strength is the unbraced length of the member. Therefore, it is critical that the tower legs are adequately braced while renovations or structural modifications are underway. Bracing must be in place to ensure the compressive stability of the tower legs and the lateral stability of the tower itself. The compressive capacity of a structural member is inversely proportional to the unbraced length. Typically, as the unbraced length of a member is increased, the compressive capacity of the member is reduced.

A representative section of the 105' tower elevation is shown in Figure 12. Figure 12 is a photograph of one of the tower bays of the top section of the tower that remained essentially intact after the collapse. The tower legs are braced by the diagonal rod members and the horizontal (appears vertical in the photograph as the tower is on its side) redundant. The typical tower bay is 10' wide by 10' tall. Therefore, this configuration of the bracing members creates unbraced lengths of five feet for the tower legs and redundant. The diagonals and the redundant were connected with two bolts at their mid-span as shown in Figure 13.



Figure 12. Representative Section from the Top of the Tower

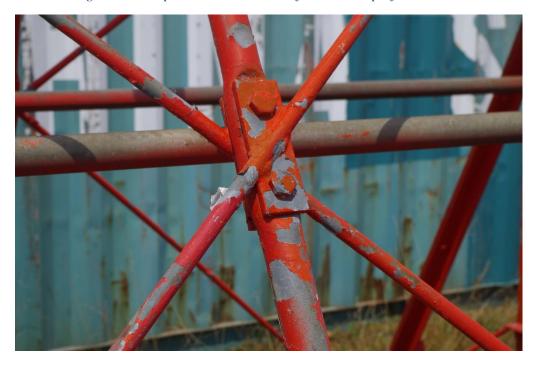


Figure 13. Bolted Connection between Diagonals and Redundant Horizontal

TCI's erection drawings states that the diagonals must be replaced one at a time. However, in order to replace a diagonal, the two bolts on each end of the diagonal and the two bolts at the diagonal's mid-span must be removed. The removal of the bolts at the mid-span, however, results in doubling the unbraced length of the tower legs and redundant from five to ten feet.

This doubling of the unbraced length creates three problems for the redundant member. First, the redundant member exceeds the allowable slenderness ratio for main compression members other than leg members and for secondary members (200 and 250 respectively) as outlined in ANSI/TIA-222-G. The resultant slenderness ratio of the redundant member without the bolted connection at its mid-span is 274. Second, the unfactored compressive resistance is reduced from 32 kips to 8 kips. This 75% reduction of compressive strength created the third problem for the redundant member. The redundant no longer satisfied the ANSI/TIA-222-G requirement for minimum bracing resistance for the tower legs. ANSI/TIA-222-G requires that the strength of the brace is at least 1.5% of the axial design compressive force of the supported member. Therefore, the unbraced length of the tower legs has doubled to ten feet.

The ANSI/TIA-222-G design strength of the tower legs was reduced by 68% due to the doubling of the unbraced length. The tower legs require a minimum bracing resistance of approximately 13 kips. However, the horizontal redundant member is only capable of providing 8 kips. The resultant unfactored design strength of the tower legs reduces from 865 kips to 279 kips. The total dead load from the guy wires and the weight of the tower above the 105-foot elevation is 316 kips. Furthermore, any incidental wind load would increase the compressive load on some of the tower legs. The overstressing of the tower legs could have been a reason for why some of the diagonals did not fit and required re-boring of the bolt holes.

The diagonal replacement procedure is described on sheet E-5 of TCI's erection drawings document and is partially shown in Figure 14. The diagonal replacement procedure requires the use of a come-a-long to eliminate the tensile forces in the diagonal to facilitate the removal of the diagonal. TCI requires the use of a come-a-long with a ten-ton capacity. However, Lemay used a come-a-long device (Griphoist/Tirfor® T-532D) with a rated working load of 8,000 pounds (4 tons). An identical model come-a-long used on-site is shown in Figure 15. The come-a-long used on the tower is shown in Figure 16 while in the debris field and which was recovered later is shown in Figure 17.

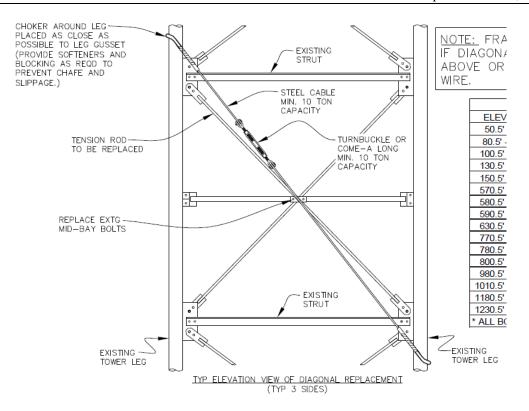


Figure 14. TCI Diagonal Replacement (E-5)



Figure 15. Lemay Come-a-long Used On-site



Figure 16. T-532D Come-a-long in Debris



Figure 17. T-532D Come-a-long Salvage from Debris

TCI's erection drawings document requires the use of a temporary frame when a diagonal is replaced above or below a guy wire location. Furthermore, TCI requires that the frame, provided by Lemay, be approved by TCI. During an interview with TCI engineering staff, TCI stated that they had no communications with Lemay about the use or design of a temporary frame. Lemay should have submitted a temporary frame design to TCI since diagonals required replacement

above guy wire levels 3, 4 and 5. Reciprocally, TCI should have requested a temporary frame design from Lemay since TCI's diagonal replacement procedure requires them to approve the frame. The notes from sheet E-5 of TCI's erection documents is shown in Figure 18. The lack of the temporary frame design did not contribute to the collapse of the communication tower, because at the time of the incident Lemay was not working on a bay that required a temporary frame.

NOTE: FRAME IS REQUIRED IF DIAGONAL IS REPLACED ABOVE OR BELOW A GUY WIRE.

NOTE:
FRAME TO BE PROVIDED
BY THE ERECTOR AND
APPROVED BY TCI

Figure 18. TCI Temporary Frame Requirements (E-5)

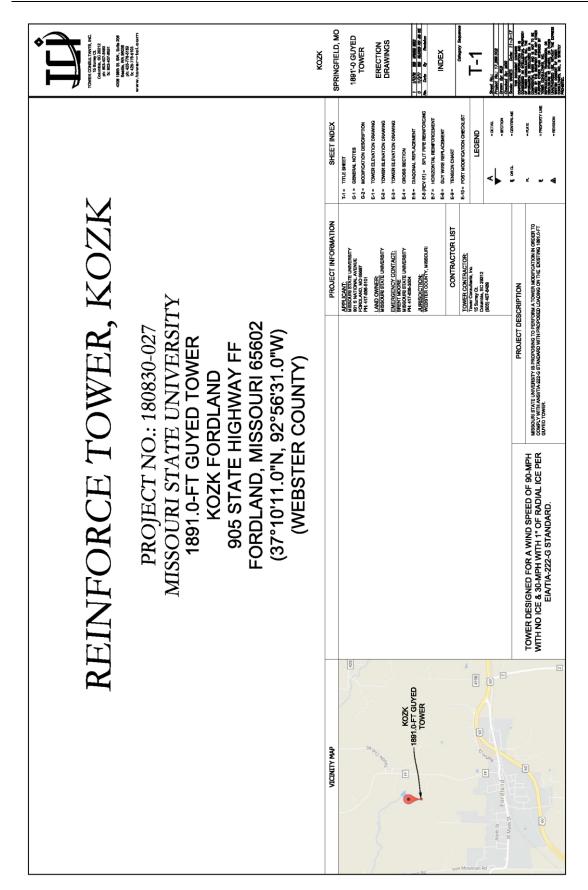
#### **Conclusion**

Based upon the above, we conclude that:

- 1) TCI's suggested diagonal replacement procedure was flawed in that it compromised the effectiveness of the integrated surrounding braces and the load bearing capacity of the tower legs. A single diagonal brace could not be removed without affecting the integrity of the redundant brace because the braces share two common bolts at the diagonal/redundant connection.
- 2) The cause of the communication tower collapse was the weakening of the compressive strength of the tower legs by removing the bolts at the connection of the diagonals to the horizontal redundant. The compromised redundant effectively doubled the unbraced length of the tower leg which reduced the compressive capacity of the tower leg.
- 3) Lemay used an undersized come-a-long while removing the diagonal braces.
- 4) Lemay failed to provide the design of the required temporary frame for diagonal replacement above or below a guy level. TCI failed to confirm the use/design of a temporary frame as TCI is required to approve the adequacy of the temporary frame prior to diagonal replacement according to TCI's construction documentation.

## Appendix A

ERECTION DRAWINGS
(PREPARED BY TCI)



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# **GENERAL NOTES**

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3. ALL DIMENSIONS, MATERIALS, AND DETAILS OF THE EXISTING STRUCTURES ARE INCLUDED FOR INFORMATION ONLY. CONTRACTORS SALT. FIELD VERIFY ALL TELELAWIN INFORMATION HORD, TO COMSTRUCTURO METABROTHOW AND NOTIFY THE ENGINEER OF PECOPO IMMEDITE OF PAY VARANCE OR DISCREPANCIES. ALL HEW WORK SHALL ACCOMMICIANTE EXISTING CONDITIONS, DETAILS NOT SPECIFICALLY SHOWN ON THE DRAWINGS SHALL FOLLOW SIMILAR DETAILS FOR THIS JOB.

4, DIMENSIONS AND ELEVATIONS GIVEN FOR THE NEW CONSTRUCTION MUST ALSO BE VERHED BY THE CONTRACTOR PRIOR TO FEBRICATION AND IESECTION TO ASSURE PROPER FIT AND ALIGNMENT OF THE STRUCTURAL COMPONENTS IN ACCORDANCE WITH THE INTENT OF THE CONTRACT DOCUMENTS.

5. ANY SUBSTITUTIONS MUST CONFORM TO THE REQUIREMENTS OF THESE NOTES AND SPECIFICATIONS AND SHOULD BE SIMILAR TO THOSE SHOWN. ALL SUBSTITUTIONS SHALL BE SUBMITTED TO THE ENGINEER OF RECORD FOR REVIEW AND APPROVAL PRIOR TO FABRICATION. 6. ANY MANUFACTIVED DISSIGNE ELBERTS MUST COAPGON. THE REQUIREBURITY OF THESE NOTTES AND SPECIFICATIONS AND SHOULD BE SMILLAY TO THOSE SHOWN. THESE DESIGNE LEBRINSTS MUST BE STAMPED BY A REGISTERED PROFESSIONAL BROWNERS. THE SECONDED COMPINATION TO PREPARE PERMI DRAWING SET SEALED BY A PROFESSIONAL BROWNERS BEING PROFF REGISTER DRAWING SHOWNERS. THE STAMP WHERE THE WORNEY BROWNERS AND THE REGISTERED BY A PROPROMAL BROWNER REGISTERED BY A PROPROMAL SAND OTHER REGISTERED BY A DEPROVAL PROFF SECONDED.

7. ALL WORK SHALL BE DONE IN ACCORDANCE WITH LOCAL CODES AND SAFETY REGULATIONS.

8. THE CONTRACTOR IS RESPONSIBLE FOR THE DESIGN AND EXECUTION OF ALL MISCELLANEOUS SHORING, BRACING, TEMPORARY SUPPORTS ETC. NECESSARY TO PROVIDE A COMPLETE AND STABLE STRUCTURE AS SHOWN ON THESE DRAWINGS, ALL INSTALLATION PROCEDURES, SAFEGUARDS AND MEANS AND MEANS AND MEANS AND MEANS OF CONSTRUCTION ARE THE SOLE RESPONSIBILITY OF THE CONTRACTOR.

B. A DETAILED RIGGING PLAN SHALL BE PREPARED BY THE CONTRACTOR AND SUBMITTED TO THE OWNER FOR APPROVAL. THE RIGGING PLAN SHALL INDOCAPACITY, DATA, WIRE ROPE SIZE AND CAPACITY RIGGING DEPACED AND SHALL SHA

APPLICABLE CODES AND STANDARDS. . ANSITIAEIA: STRUCTURAL STANDARDS FOR STEEL ANTENNA TOWERS AND ANTENNA SUPPORTING STRUCTURES.

2. IBC: INTERNATIONAL BUILDING CODE, LATEST EDITION.

3. ASTM: STANDARDS FOR BUILDING CODES, LATEST EDITION.

4. ACI 318: AMERICAN CONCRETE INSTITUTE, BUILDING CODE REQUIREMENTS FOR STRUCTURAL CONCRETE, LATEST EDITION.

5. ACI 315: AMERICAN CONCRETE INSTITUTE, DETAILS AND DETAILING OF CONCRETE REINFORCEMENT, LATEST EDITION.

6. CSRI: CONCRETE STEEL REINFORCING INSTITUTE, MANUAL OF STANDARD PRACTICE, LATEST EDITION.

7. AISC: AMERICAN INSTITUTE OF STEEL CONSTRUCTION, MANUAL OF STEEL CONSTRUCTION, LATEST EDITION.

8. AWS: AMERICAN WELDING SOCIETY, STRUCTURAL WELDING CODE, LATEST EDITION.

STEEL AND FABRICATION.
1. ALI STEEL FARRICATION TO BE DONE BY AN AISC CERTIFIED FABRICATION FACILITY IN ACCORDANCE WITH THE LATEST EDITION OF THE ARRENCAN INSTITUTE OF STEEL CONSTRUCTION. 2. ALL STEEL TO BE ASTM A572 GR.50 (50KS) MIN YIELD STRENGTH) U.N.O.; BOLTS TO BE ASTM A325 WITH ANCO LOCKNUTS U.N.O.

3. ALL MATERIAL TO BE HOT DIPPED GALVANIZED PER ASTM A123 OR ASTM A153.

4. BOLT HOLE DIAMETER SHALL NOT BE MORE THAN 1% LARGER THAN NOMINAL BOLT DIAMETER AND SHALL BE PUNCHED OR DRILLED UN.O.

3. MINIMUM WELD SIZE TO BE 0.3125 INCH FILLET WELDS UNLESS NOTED OTHERWISE ON THE DRAWINGS. 2. ALL ELECTRODES TO BE E70 LOW HYDROGEN TYPE.

4. ALL WELDED CONNECTIONS TO BE SEAL WELDED FOR GALVANIZING.

T<u>RELD INSTALLATION</u> 1. ALL GALVANIZED SURFACE THAT ARE SCRATCHED OR DAMAGED SHALL BE REPAIRED USING A ZINC RICH TWO PART EPOXY SUCH AS CARBOLINE 15 OR COUNTAIETT.

2. ARD BOLTS SHALL BE SPRAY PAINTED WITH A COAT OF COLD GALVANIZING PRIOR TO INSTALLATION FOLLOWED BY A COAT OF A ZINC RICH TWO PART EPOXY SUCH AS CARBOLINE 15 OR EQUIVALENT AFTER INSTALLATION.

3. HARDWARE INTERFERING WITH THE INSTALLATION OF REINFORCING MATERIAL SHALL BE TEMPORARILY MOVED AND REINSTALLED AFTER THE COMPLETION OF THE WORK.

4. WHEN FIELD WELDING IS REQUIRED THE STEEL SHALL BE CLEANED OF ALL PAINT AND GALVANIZING TO A BARE METAL AS SPECIFIED PER AWS D1.1. PREHEATING AND POST HEATING MAY BE REQUIRED.

5. WELDED AREAS ARE TO BE TOUCHED UP USING A ZINC RICH TWO PART EPOXY SUCH AS CARBOLINE 15 OR EQUIVALENT.

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FOUNDATIONS 1. CONTRACTOR SHALL VERIEY THE LOCATION OF UNDERGROUND UTILITIES IN THE AREA WHERE THE WORK IS TO BE PERFORMED.

2. DRILLED SHAFT INSTALLED IN ACCORDANCE WITH ACI-336 (LATEST EDITION).

<u>CONCRETE</u> I. ALL CONCRETE FOR FOUNDATIONS SHALL HAVE A MINIMIUM COMPRESSIVE STRENGTH OF 4000 PSI, AFTER 28 DAYS.

2. THE CONCRETE MIX SHALL NOT CONTAIN LESS THAN 52 SACKS OF CEMENT (ASTM C 150 TYPE II) PER CUBIC YARD.

4. THE CONCRETE MIX SHALL PRODUCE A MAXIMUM SLUMP OF 5" ±1".

3. THE CONCRETE SHALL HAVE A MAXIMUM AGGREGATE SIZE OF  $\frac{7}{8}.$ 

S. THE CONCRETE MIX SHALL HAVE A TOTAL AIR CONTENT OF 5%, WITH A TOLERANCE OF PLUS OR MINUS 1.5%, AIR-ENTRAINING ADMIXTURES SHALL CONFORM TO ASTIN C'260.

B. THE CONCRETE MIX SHALL HAVE A MAXIMUM WATER-CEMENT RATIO OF 0.45, WATER REDUCING OR ACCELERATING ADMIXTURES SHALL CONFORM TO ASTIM C. 484. . THE CONCRETE SHALL NOT CONTAIN CALCIUM CHLORIDE OR ANY OTHER ADMIXTURE CONTAINING CHLORIDE OTHER THAN NATURAL IMPURITIES.

8. FORM WORK SHALL CONFORM TO ACI 318 (LATEST EDITION) SPECIFICATIONS.

9. ALL CONCRETE SHALL BE PLACED IN A MONOLITHIC POUR UNLESS SHOWN OTHERWISE ON THE DRAWINGS.

10. PROVIDE CHAMFERS AT ALL EXPOSED CORNERS OF CONCRETE.

11. CONCRETE WORK UNDER EXTREME WEATHER CONDITIONS SHALL CONFORM TO ACI 318 (LATEST EDITION) SPECIFICATIONS

STEEL REINFORCEMENT (REBAR) . ALL REINFORCING STEEL TO BE GRADE 60 DEFORMED BILLET STEEL PER ASTM A616.

2. REINFORCEMENT SHALL BE FABRICATED AND PLACED IN ACCORDANCE WITH THE ACI 315 AND CSRI. SUPPORT REINFORCING AS REQUIRED BY CSRI TO PREVENT DISPLACEMENT UPON CONCRETE POURING.

3. MAINTAIN ALL CLEARANCES NOTED ON THE DRAWINGS. WHERE NO DIMENSIONS ARE NOTED, USE THE ACI RECOMMENDED CLEARANCES. 4. FOR CONCRETE POURED AGAINST SOIL, THE MINIMUM COVER FOR ALL REINFORCING BARS SHALL BE 3".

3. ALL WELDED WIPE FABRIC TO BE PER ASTM A185. ALL BARS AND WIRE SHALL BE FREE OF FUSIT, MILL SCALE, DIRT, OR OTHER FOREIGN MATERIAL PRIOR TO CASTING CONCRETE.

5. TIE BARS SECURELY WITH #16 ANNEALED WIRE AND SUPPORT AS REQUIRED.

7. PROVIDE MINIMUM LAP SPLICES OF 36 BAR DIAMETERS UNLESS NOTED OTHERWISE.

9. FIELD BENDING OF REINFORCEMENT BARS IS NOT PERMITTED. DO NOT NELD REINFORCING BARS.

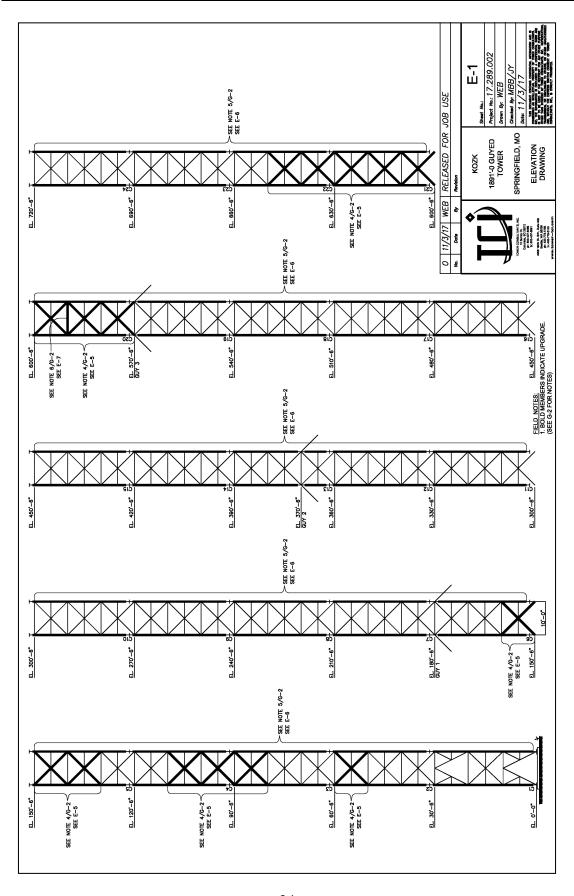
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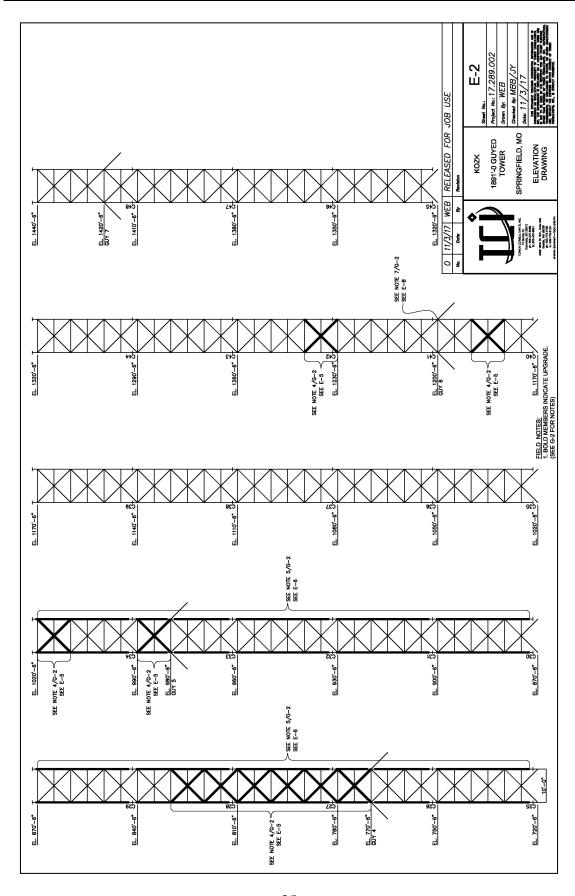
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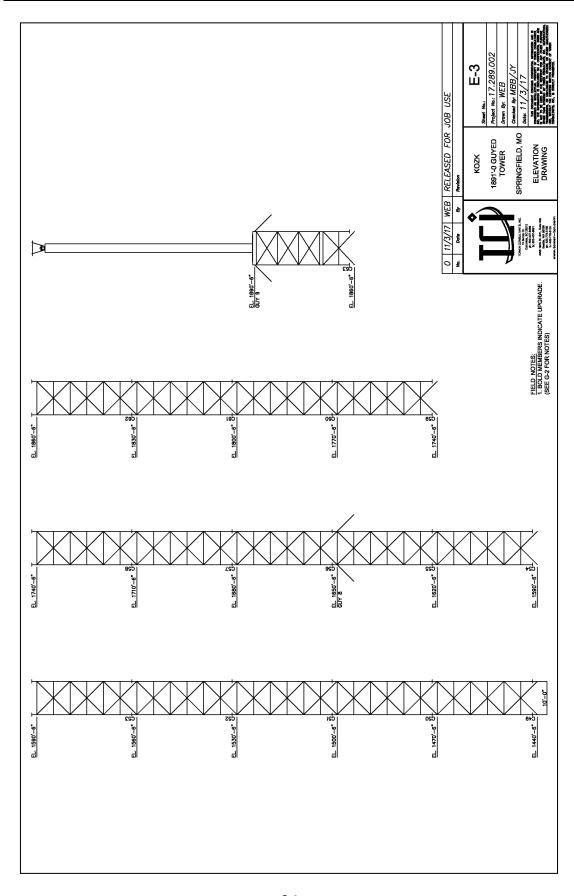
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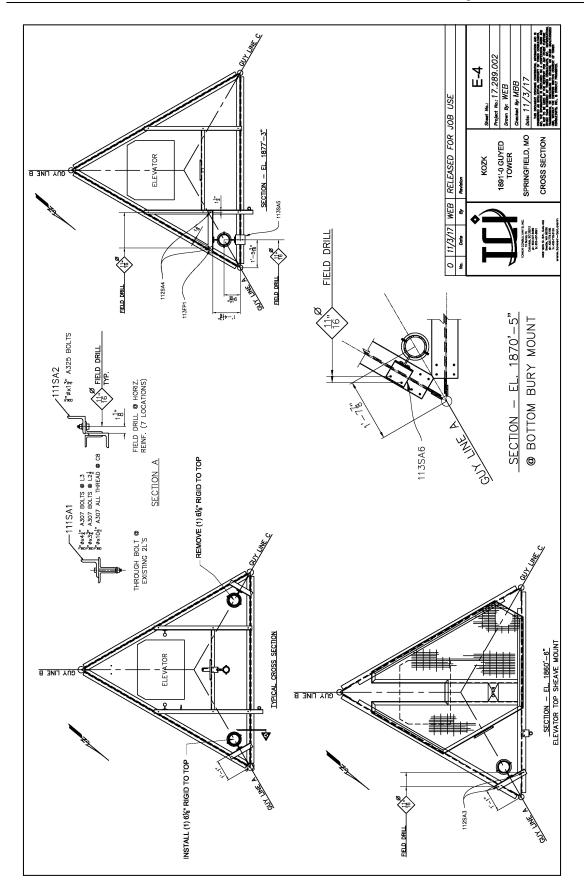
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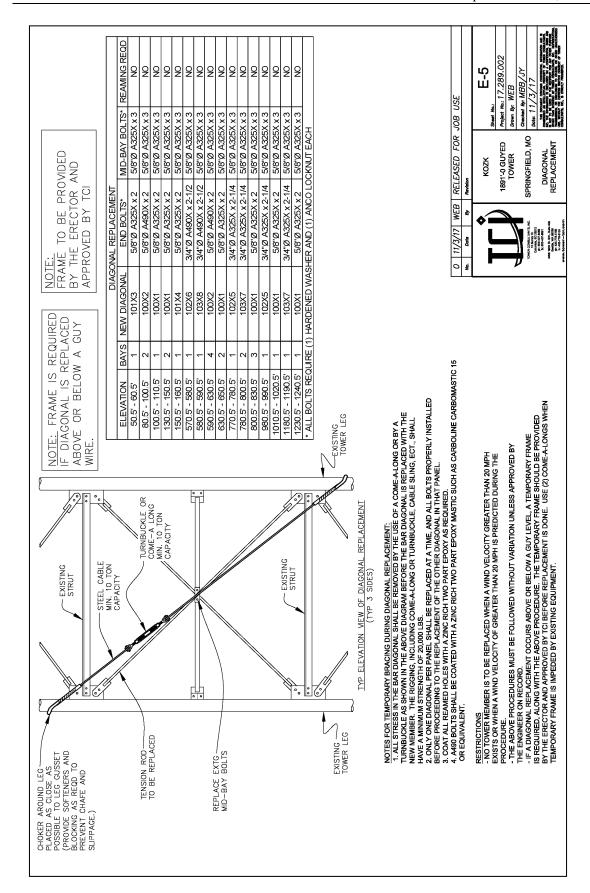
7 DEPARACE GLIV LEVEL 6, AND ADJUST THE GLIV WIRE INITIAL TENSION LISTING THE TANGENT	INTERCEPT METHOD TO THE VALUES LISTED IN THE CHART BELOW. REUSE EXISTING GROUNDING AND HTD (SEE E-8 & E-9):	Control   Cont	NOTE: VALUES SHOWN ABOVE ARE VALID AT 60 DEGREES FAHRENHEIT; A PAT CHART WITH TEMPERATURE CORRECTIONS WILL BE REQUIRED FOR FIELD ADJUSTMENTS  8. ALL MATERIAL SHALL BE HOT DIP GALVANIZED IN ACCORDANCE TO ASTM SPECIFICATIONS.  9. ALL REINFORCING MATERIAL SHALL BE PAINTED IN THE FIELD TO MATCH THE EXISTING COLOR SCHEME OF THE TOWER.  10. THE MODIFICATION MATERIAL AND INSTALLATION DRAWINGS CONTAINED HEREIN ARE BASED ON THE ASSUMPTION THAT THE TOWER HAS BEEN PROPERLY INSTALLED AND MAINTAINED, INCLUDING BUT NOT LIMITED TO THE FOLLOWING: A. RROPER ALIGNMENT AND PLUMBNESS. B. CORRECT BOLT TIGHTNESS. C. CORRECT BOLT TIGHTNESS. D. NO SIGNIFICANT DETERIORATION OR DAMAGE TO ANY COMPONENT.  11. ALL MATERIAL REQUIRED BY SHEETS E-1 THROUGH E-8 FURNISHED TO CONTRACTOR BY TEL. FOR PRICTING PLASE CONTACT:	RON DOZSA 425-778-5169  DESIGN INFORMATION:  1. THIS DRAWING PACKAGE IS BASED ON TOWER CONSULTANTS ANALYSIS REPORT 17.289.001, DATED MAY 19, 201.  2. THE TOWER IS DESIGNED FOR THE EXISTING AND PROPOSED LOADING AS LISTED IN THE REPORT	REFERENCED ABOVE.  ANTENNA WORK:  1. REMOVE THE FOLLOWING LINES (SEE CROSS SECTION ON E-4):  No. Park 18 RELEASED FOR JOB USE No. Park 18 RELEASED FOR JOB USE No. Park 18 RELEASED FOR JOB USE	The state of the s
MODIFICATION DESCRIPTION:	1. ITLS DRAWING IS FOR JOB USE. 2. UPGRADES APPLY TO ALL THREE FACES OF THE TOWER.	3. A TEMPORARY BRACE MUST BE INSTALLED THAT IS OF EQUIVALENT OR GREATER CAPACITY THAN THE MINIBER BEING REPLACED. THE TEMPORARY BRACE SHALL BE PLACED ADJACENT TO THE MEMBER BEING REPLACED SUCH THAT IT WILL TAKE THE LOAD AFTER THE EXISTING MEMBER IS REMOVED.  A TEMPORARY FRAME IS REQUIRED. ABOVE AND BELOW GUY LEVELS DURING DIAGONAL. REPLACEMENT.  4. REPLACEMENT.  4. REPLACE THE EXISTING SOLID ROD DIAGONAL MEMBERS WITH A NEW HIGHER CAPACITY MEMBER AT THE FOLLOWING LOCATIONS (SEE E-5):	(18AY) (25 (28AYS) (25 (18AY) (25 (18AY) (25 (28AYS) (	0.0 - 0.05 (\$ SECTIONS) HATH YES 5.25 'O.D. × 0.5" WALL, PF-SIOKS MIN. 60.5 - 150.5 (\$ SECTIONS) HATH YES 5.25 'O.D. × 0.5" WALL, PF-SIOKS MIN. 210.5 - 210.5 (\$ SECTIONS) HATH YES 5.25 'O.D. × 0.5" WALL, PF-SIOKS MIN. 210.5 - 300.5 (\$ SECTIONS) HATH YES 5.25 'O.D. × 0.5" WALL, PF-SIOKS MIN. 300.5 - 420.5 (\$ SECTION) HATH YES 5.25 'O.D. × 0.5" WALL, PF-SIOKS MIN. 420.5 - 420.5 (\$ SECTION) HATH YES 5.25 'O.D. × 0.5" WALL, PF-SIOKSI MIN. 420.5 - 600.5 (\$ SECTION) HATH YES 5.125 'O.D. × 0.5" WALL, PF-SIOKSI MIN. 420.5 - 600.5 (\$ SECTIONS) HATH YES 5.125 'O.D. × 0.5" WALL, PF-SIOKSI MIN. 600.5 - 810.5 (\$ SECTIONS) HATH YES 5.125 'O.D. × 0.5" WALL, PF-SIOKSI MIN. 810.5 - 10.20.5 (\$ SECTIONS) HATH YES 4.875 'O.D. × 0.5" WALL, PF-SIOKSI MIN. 810.5 - 10.20.5 (\$ SECTIONS) HATH YES 4.75" O.D. × 0.5" WALL, PF-SIOKSI MIN. 810.5 - 10.20.5 (\$ SECTIONS) HATH YES 4.75" O.D. × 0.5" WALL, PF-SIOKSI MIN. 810.5 - 10.20.5 (\$ SECTIONS) HATH YES 4.75" O.D. × 0.5" WALL, PF-SIOKSI MIN. 810.5 - 10.20.5 (\$ SECTIONS) HATH YES 4.75" O.D. × 0.5" WALL, PF-SIOKSI MIN. 810.5 - 10.20.5 (\$ SECTIONS) HATH YES 4.75" O.D. × 0.5" WALL, PF-SIOKSI MIN. 810.5 - 10.20.5 (\$ SECTIONS) HATH YES 4.75" O.D. × 0.5" WALL, PF-SIOKSI MIN. 810.5 - 10.20.5 (\$ SECTIONS) HATH YES 4.75" O.D. × 0.5" WALL, PF-SIOKSI MIN. 810.5 - 10.20.5 (\$ SECTIONS) HATH YES 4.75" O.D. × 0.5" WALL, PF-SIOKSI MIN. 810.5 - 10.20.5 (\$ SECTIONS) HATH YES 4.75" O.D. × 0.5" WALL, PF-SIOKSI MIN. 810.5 - 10.20.5 (\$ SECTIONS) HATH YES 4.75" O.D. × 0.5" WALL, PF-SIOKSI MIN. 810.5 - 10.20.5 (\$ SECTIONS) HATH YES 4.75" O.D. × 0.5" WALL, PF-SIOKSI MIN. 810.5 - 10.20.5 (\$ SECTIONS) HATH YES 4.75" O.D. × 0.5" WALL, PF-SIOKSI MIN. 810.5 - 10.20.5 (\$ SECTIONS) HATH YES 4.75" O.D. × 0.5" WALL, PF-SIOKSI MIN. 810.5 - 10.20.5 (\$ SECTIONS) HATH YES 4.75" O.D. × 0.5" WALL, PF-SIOKSI MIN. 810.5 - 10.20.5 (\$ SECTIONS) HATH YES 4.75" O.D. × 0.5" WALL, PF-SIOKSI MIN. 810.5 - 10.20.5 (\$ SECTIONS) HATH YES 4.75" O.D. × 0.5" WALL, PF-SIOKSI WIN. 810.5 (\$ SECTIONS) HATH YES 4.75" O.D. × 0.5" WALL, PF-SIOKSI WIN. 90.	6. KEINFORCE THE EXISTING DOUBLE ANGLE ADMICTON AL MEMBERS BY AUDING A SINGLE ANGLE MEMBER BETWEEN THE DOUBLE ANGLES AT THE FOLLOWING LOCATIONS (SEE E-7): 590.5" (1 LEVEL) L3½x2½x3½, ¾, № A225X BOLTS	

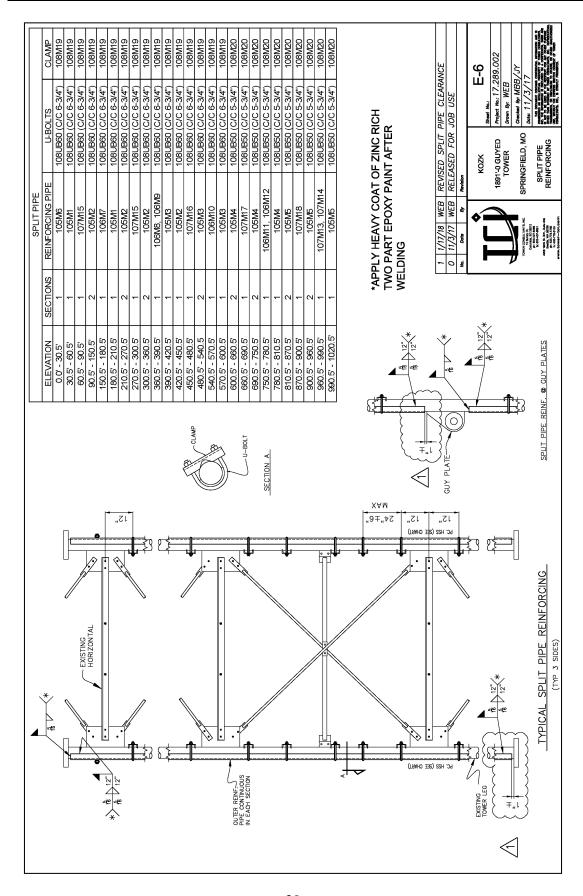


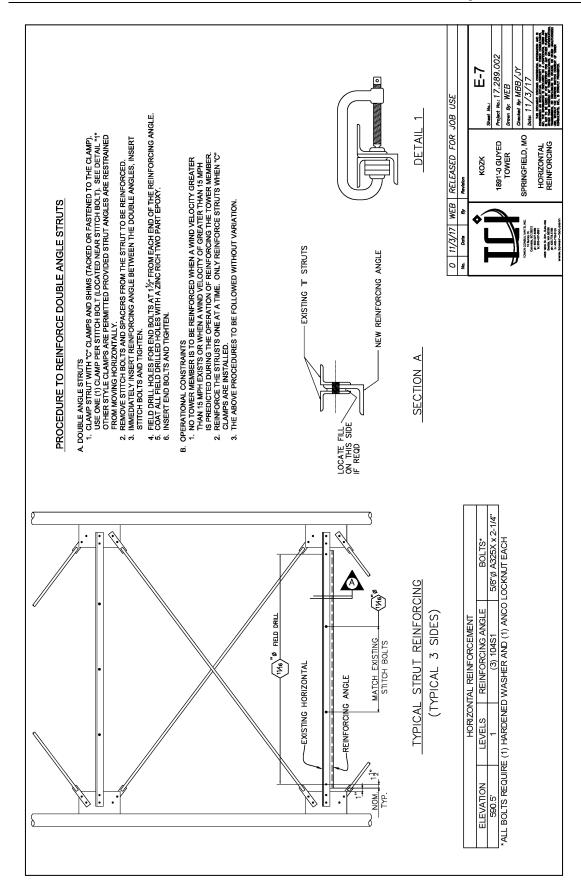


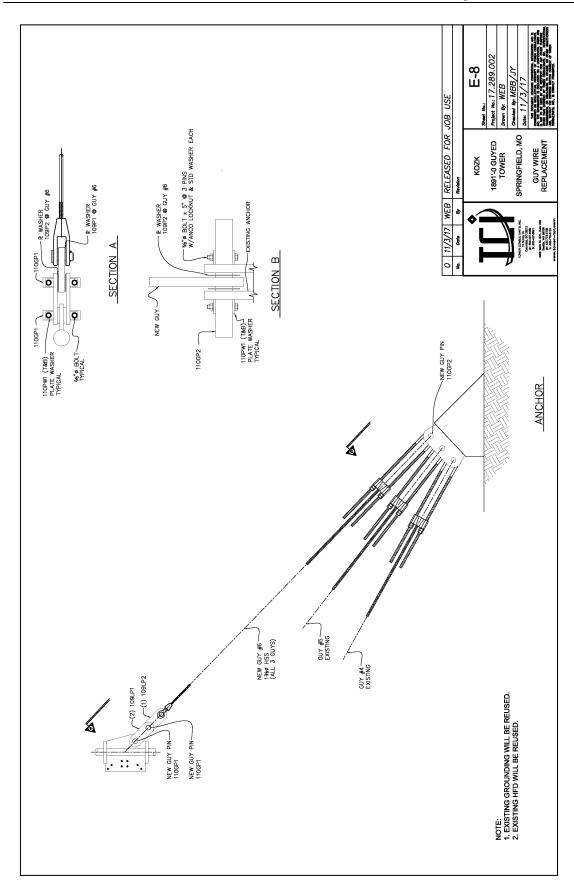


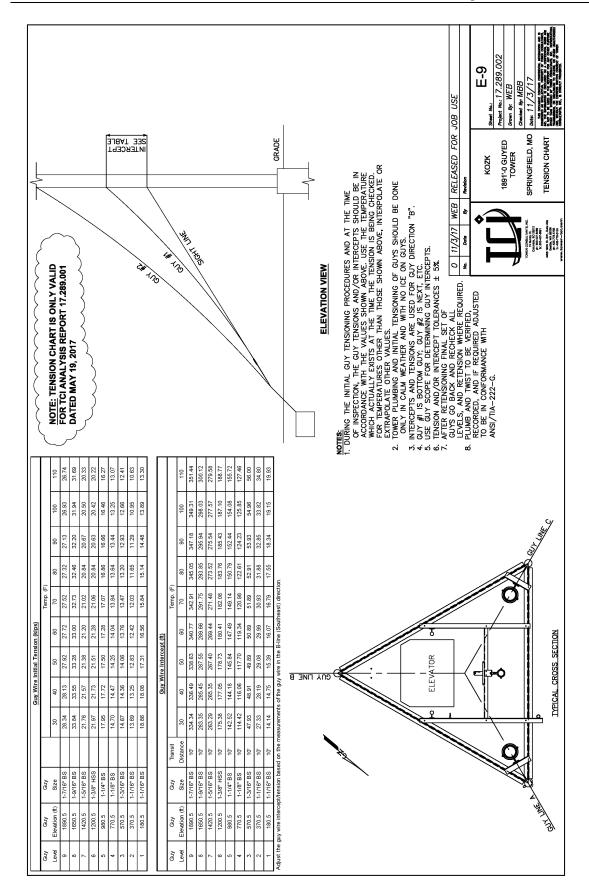








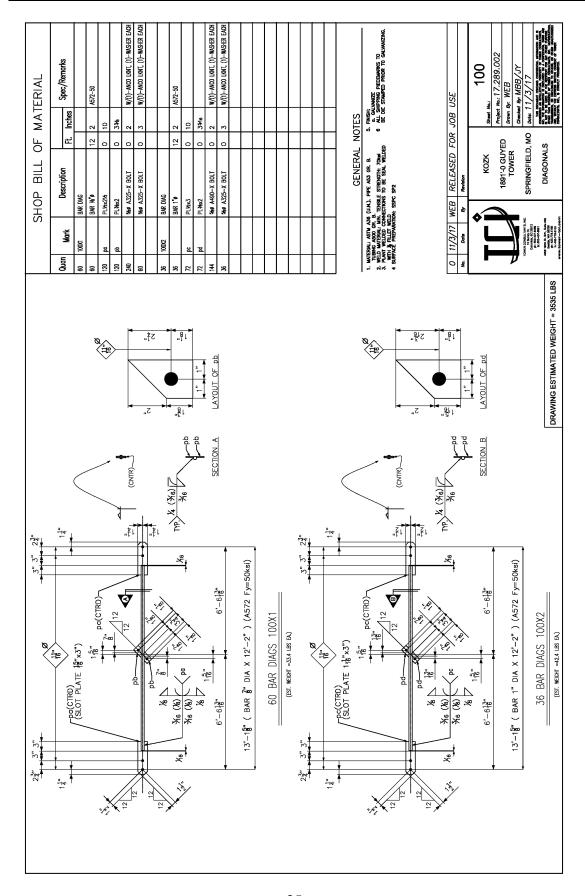


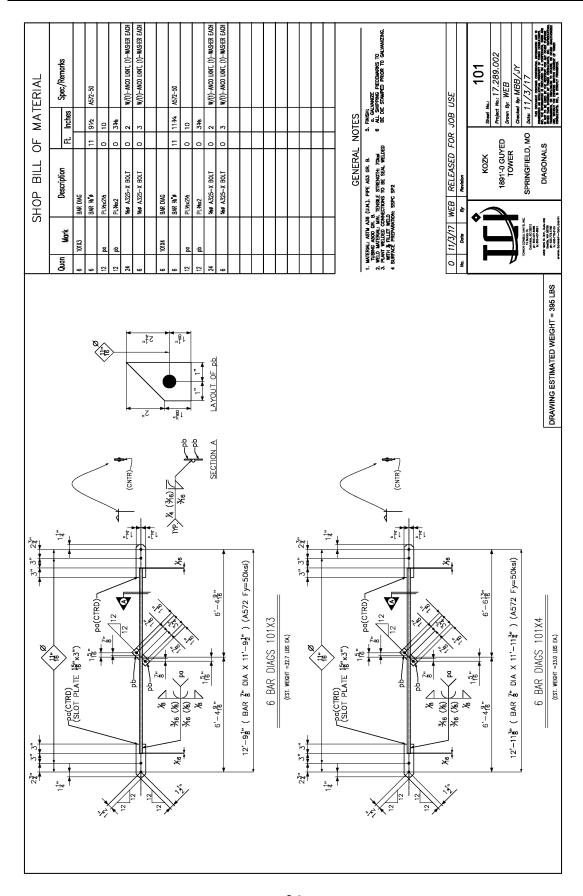


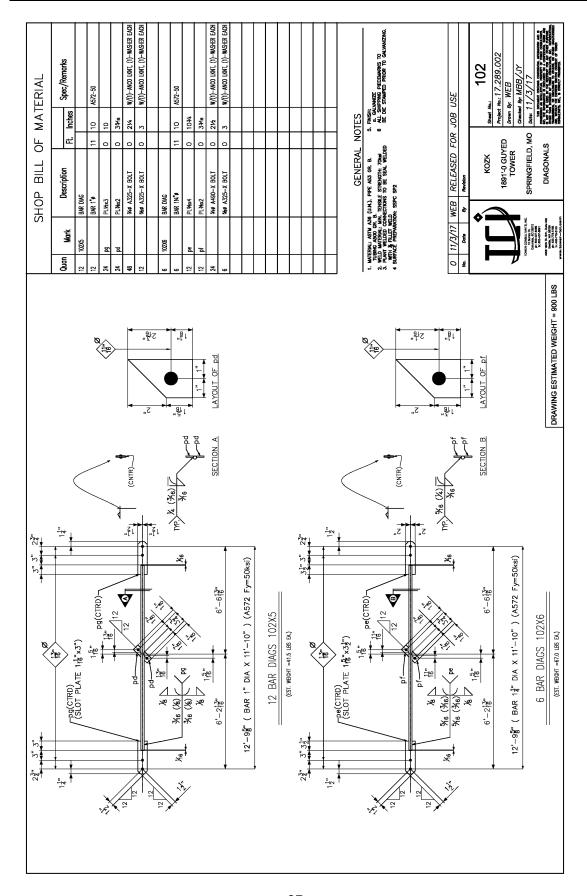
CANCELATION OR DELAYS IN SCHEDULED MI		OOSIS, FEEL, LOSS OF BEDOSITS AND/ON OHITE PARALITE RELALED TO THE CANCELLATION ON DELAY INCLINED BY ETHER PARTY FOR ANY TITE (E.G., TRAKEL AND L.COGNIG, COSTS OF KEEPING EQUIPMENT ON—STE, ETC.). IF TCI CONTRACTS DIRECTLY		CORRECTION OF FAILING WIS. THE MODERATION RESILIENT WOULD FAIL THE MI (FAILED MI), THE OC SHALL WORK WITH GUSTOMER TO COORDINATE, A REMEDATION PAIN IN ONE OF TWO WAYS:				ALL VERFICATION INSPECTIONS SYALL BE HELD TO THE SAME SPECIFICATIONS AND REQUIREMENTS IN THE CONTRACT DOCUMENTS.	YERIKATINI RISPULINI MAT BE COMPULED BT AN RUCEPURENT INSET YOR MATER A MODIFICATION PROJECT IS COMPULED. AS LANKED BY THE DATE OF AN ACCEPTED "PASSING ME, OR "PASS AS LIGITED ME. REPORT FOR THE ORIGINAL PROJECT.		* PRE-CONSTINCTION SERENA, SIT CANDITION  * PHOTOGRAPHS DURING THE REPIPENCEMENT MODIFICATION CONSTRUCTION/ERECTION  * AND INSECTION MODIFICATION CONTINUES AND MODIFICATION CONSTRUCTION CONTINUES AND CONTINUES AN	FOUND IN MODIFICATIONS     FINAL INSTALLED CONDITION     POST CONSTRUCTION PHOTOGRAPHS	** FINAL INFELD CONDITION PHOTOS OF ELEVATED MODIFICATIONS TAKEN FROM THE GROUND SHALL BE CONSIDERED	NADEGNATE.			<b>.</b>							0   11/3/17   WEB   RELEASED FOR JOB USE	Date By Revision	◆ kozk E-10	1891-0 GUYED Sheet No.: 17 280 002	TOWER	SPRINGFIELD, MO	POST	THE COLUMN TO THE COLUMN THE COLU
MODIFICATION INSPECTION NOTES.	GENERAL The Modification Inspection (MI) is a visual inspection of tower modifications	AND A REMENY OF CONSTRUCTION INSPECTIONS AND OTHER REDORTS IN ENSURE THE INSTALLATION WAS CONSTRUCTED IN ACCORDANCE WITH THE CONTRACT DOCUMENTS, NAMELY THE MODIFICATION DRAWINGS, AS DESIGNED BY THE ENGINEER OF RECORD (EOR).	THE MISTO COMPRAINING TALLATION COMPIGURATION AND WORGALANISHIP ONLY AND IS TWO A REVIEW OF THE MODIFICATION DESIGN. THE THISELF, NOW THE STRUCTURAL COMPENSING OF THE STRUCTURAL.	MODIFICATION DESIGN EFFECTIVENESS AND INTEGRITY RESIDES WITH THE EOR AT ALL TIMES.	ALL MESSAGE BETTER THE CHARLES AND THE CHARLES	COORDINATING AS SOON AS A PO INTECEDING. IN INTERCOMMENTARION FIND AND AND COORDINATING AS SOON AS A PO INTECEDING. IN INTECHAND FURTH WILL BE PROACTIVE IN REACHING OUT TO THE OTHER PARTY.	MESPECTOR THE MINISCECTOR IS REQUIRED TO CONTACT THE GC AS SOOM AS RECEIVING A PO FOR THE MI TO, AT A MAINIMUM:	<ul> <li>REVIEW THE REQUIREMENTS OF THE MI CHECKLIST</li> <li>WORK WITH THE GG TO DEBLOOP A SCHEDULE TO CONDUCT ON—SITE INSPECTIONS, INCLIDING FOCKINATION INSPECTIONS.</li> </ul>	THE MI INSPECTION IS RESPONSIBLE FOR COLLECTING ALL GENERAL CONTRACTOR (GC) THE MI INSPECTION AND TEST PEPDORS BY SEVENING THE DIGITALISTS FOR ADJUSTMENTS TO THE	CONTRACT DOCUMENTS, CONDUCTING THE IN-PIELD INSPECTIONS, AND SUBMITTING THI GENERAL CONTRACTOR.	FF	<ul> <li>WORK WITH THE MI INSPECTIOR TO DEVELOP A SCHEDULE TO CONDUCT ON—SITE INSPECTIONS, INCLUDING FOUNDATION INSPECTIONS</li> <li>BETTER UNDERSYAND ALL INSPECTION AND TESTING REQUIREMENTS</li> </ul>	F-		ш			THE FOUNDATION INSPECTIONS TO ALLOW FOUNDATION AND MI INSPECTION(S) TO COMMENCE WITH ONE SITE WIST.  IT IS PREPERFORED TO HAVE THE GC AND, MI INSPECTOR ON-SITE DURING THE MI TO													
	BRIEF DESCRIPTION (SEE ENG-SOW-10007)	PRE-CONSTRUCTION THIS CHECKLIST SHALL BE INCLUDED IN THE MI REPORT	FABRICATION DRAWINGS SHALL BE SUBMITTED TO THE ENGINEER OF RECORD FOR REVER. THE CONTRACTOR SHALL BROWDE THE APPROVED SHOP DRAWINGS TO THE MI INSPECTIOR FOR INCLUSION IN THE LI REPORT.	A LETTER FROM THE FABRICATOR, STATING THAT THE WORK WAS PERFORMED IN ACCORDANCE WITH MOUSTRY STAVANDARS AND THE CONTROLT DOCUMENTS SHALL BE PROVIDED TO THE MI NEPECTRY FOR INCLUSION IN THE MI REPORT.	CRITICAL SHOP MEDS THAT REQUIRE TESTING AFE MEDIO ON THESE CONTRACT AND A CRITICAL SHOULD INSPECTIVE SHALL PERFORM INCH-DESTRUCTIVE. TESTING AND A REPORT SHALL BE PROVIDED TO THE MI INSPECTOR FOR INCLUSION IN THE MI REPORT.	MIL CERTEICATION SAAL BE PROVIDED FOR ALL STEEL WITH A YIELD STRENGTH GREATER THAN 36 KES AND THE SOCKLIBERTATION SHALL BE PROVIDED TO THE MINSPECTOR FOR MICLISORN IN THE MI REPORT.	A WSJAL OBSERVATION OF A PORTION OF THE EXISTING STRUCTURE (AS NOTED ON THESE DRAWNGS) IS REQUIRED AND A WRITTEN REPORT SHALL BE PROVIDED TO THE MI NEPECTOR FOR NOLUSION IN THE MI REPORT.	A VISUAL OBSERVATION OF THE POLE TO BASE PLATE CONNECTION IS REQUIRED AND A WHITTEN REPORT SHALL BE PROVIDED TO THE MI INSPECTOR FOR INCLUSION IN THE MI REPORT.	THE MATERIAL SHIPPING UST SHALL BE PROWDED TO THE MI INSPECTOR FOR INCLUSION IN THE MI REPORT.  CANCITOLING	N. LETER FROM THE GENERAL CONTRACTOR STATING THAT THE WORKHANSHIP WAS DEFENDED IN A LOCORRACE WHI PRODESTRY STANDARDS AND THESE CONTRACT PROPERTIES SHALL BE PROVIDED TO THE MI INSPECTOR FOR NOLLISON IN THE MI DEMINISTER SHALL BE PROVIDED.	A YISJAL OSERVATION OF THE EXCAVATION AND REBAR SHALL BE PERFORMED BEFORE PLADUR THE CONCRETE. A MATITED REPORT SHALL BE PROVIDED TO THE MI IMPRECINE FOR INCLUSION IN THE MI REPORT.	THE CONCRETE MIX DESIGN, SLUMP TEST, AND COMPRESSIVE STRENGTH TESTS SHALL BE PROVIDED TO THE MI INSPECTOR FOR INCLUSION IN THE MI REPORT.	POST INSTALLED ANCHOR ROD VERBICATION SHALL BE PERFORMED IN ACCORDANCE WITH CROWN REQUIREMENTS AND A REPORT SHALL BE PROVIDED TO THE MINSTECTOR FOR INCLUSION IN THE MINREPORT.	A LETTER FROM THE CASHEAL CONTRACTOR SHALL BE PROVIDED TO THE MI INSPECTOR THAT CERTIFIES THAT THE GROUT WAS INSTALLED IN ACCORDANCE WITH STANDARD INJUSTIF PRACTICES FOR INCLUSION IN THE MI REPORT.	AE CRRITIED WED INSPECTOR SHALL INSPECT AND TEST AS NECESSARY ALL FIELD WELDS AND A REPORT SHALL BE PROVIDED TO THE MI INSPECTOR FOR INCLUSION IN THE MI REPORT.	FOUNDATION SUB-CRADES SHALL BE INSPECTED AND APPROVED BY A GEOTECHNICAL ENGINEER AND A REPORT SHALL BE PROVIDED TO THE MI INSPECTOR FOR INCLUSION IN THE MI REPORT.	THE GENERAL CONTRACTOR SHALL PROVIDE DOCUMENTATION TO THE MI INSPECTOR VERFARK THAT ANY ON-SITE COLD GALVANIZACION WAS APPRIADED IN ACCORDANCE WITH STANDARD NOVETRY PRACTICES.	THE GENERAL CONTRACTION SHALL PROVIDE A REPORT TO THE REPORTION IN INSPECTION IN INFORMATION IN THE INFORMATION IN THE CHARLE FOR MICLISION IN THE GENERAL CONTRACTION SHALL IS INDIAL A CYDY OF THE CANTRACTION SHALLS.	ETHER STATING "HISTALLED AS DESIGNED" OR NOTING ANY CHANGES THAT WERE PREQUED AND APPROVED BY THE ENGINEER OF RECORD DUE TO FIELD CONDITIONS.  DACET AARLESTICATION.	THE MI INSPECTOR SHALL OBSERVE AND REPORT ANY DISOREPANCIES BETWEEN THE CONTRACTORS REDUINE DRAWING AND THE ACTUAL COMPLETED INSTALLATION.	POST-INSTALLED ANCHOR RODS SHALL BE TESTED AND A REPORT SHALL BE PROVIDED TO THE MI INSPECTOR FOR INCLUSION IN THE MI REPORT.	PHOTOGRAPHS SHALL BE SUBMITTED TO THE MI WHICH DOCUMENT PHASES OF THE CONSTITUCION. THE WINDS SHALL BE DROAMIZED IN A MANNER THAT EASILY IDENTIFES THE EXACT LOCATION OF THE PHOTO.	Port 3 for the MI report								
		1										H AND		ICATION						OR RECORD	10R ROD		OR THE MI REP. NOT REQUIRED								
POST-MODIF	REPORT ITEM	MI CHECKLIST DRAWING	EOR APPROVED SHOP DRAWINGS	FABRICATION INSPECTION	FABRICATOR CERTIFIED WELD INSPECTION	MATERIAL TEST REPORT (MTR)	FABRICATOR NDE INSPECTION	NDE REPORT OF MONOPOLE BASE PLATE (AS REQUIRED)	PACKING SLIPS	CONSTRUCTION INSPECTIONS	FOUNDATION INSPECTIONS	CONCRETE COMP. STRENGTH AND SLUMP TESTS	POST INSTALLED ANCHOR ROD VERIFICATION	BASE PLATE GROUT VERIFICATION	CONTRACTOR'S CERTIFIED WELD INSPECTION	EARTHWORK: LIFT AND DENSITY	on site cold galvanizing Verification	GUY WRE TENSION REPORT	GC AS-BUILT DOCUMENTS	MI INSPECTOR REDLINE OR RECORD DRAWING(S)	POST INSTALLED ANCHOR ROD PULL-OUT TESTING	PHOTOGRAPHS	note: X denotes a document needed for the MI report na denotes a document that is not required for the MI report								

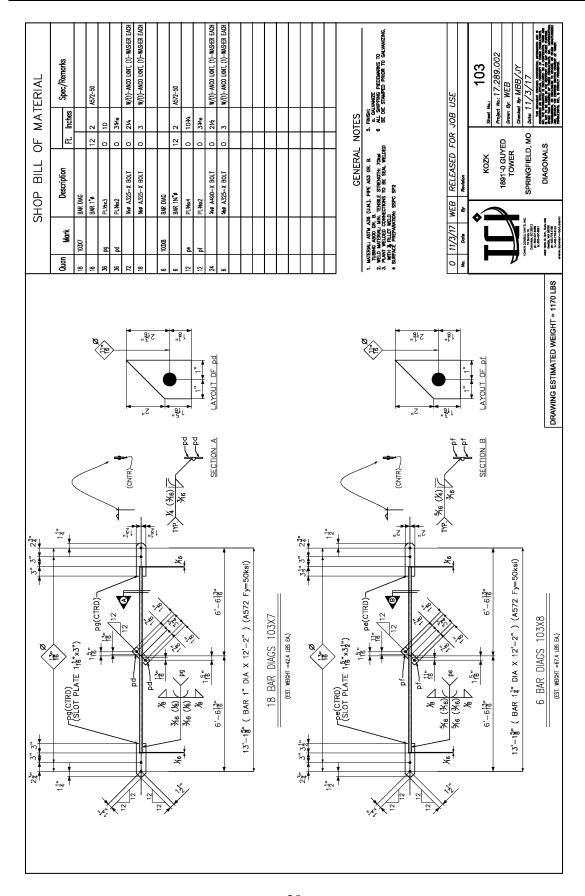
# Appendix B

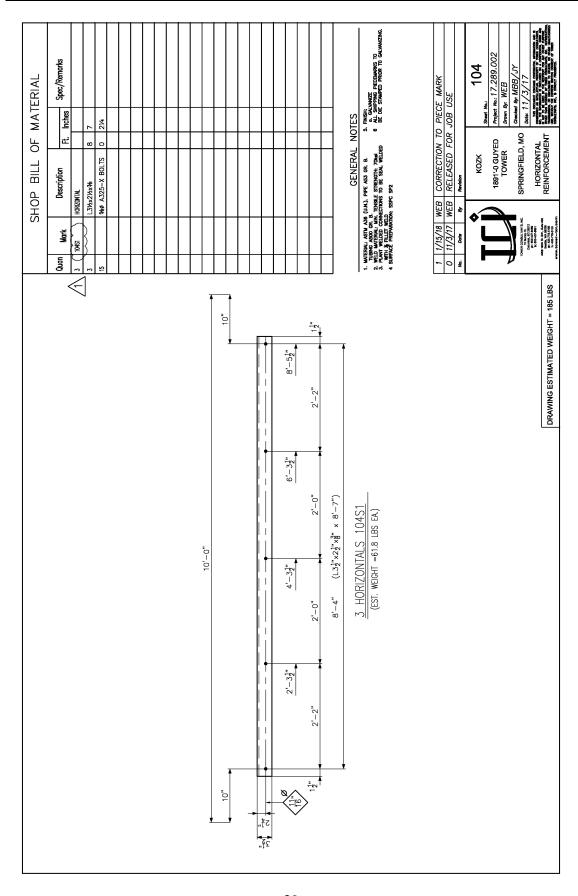
FABRICATION DRAWINGS
(PREPARED BY TCI)

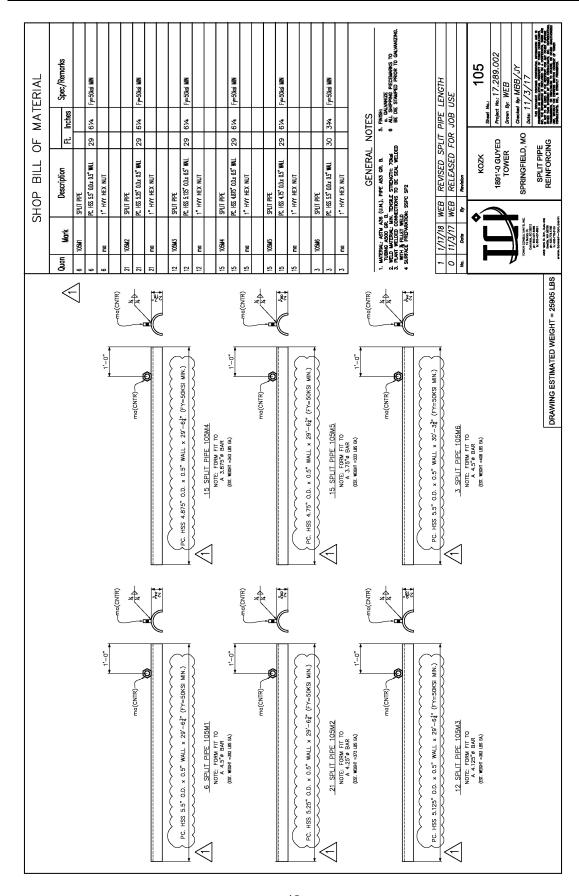


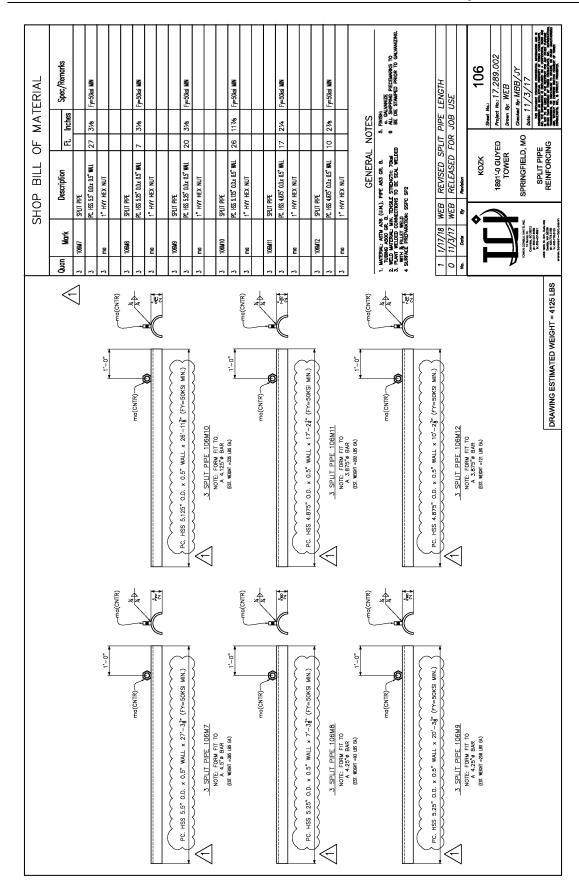


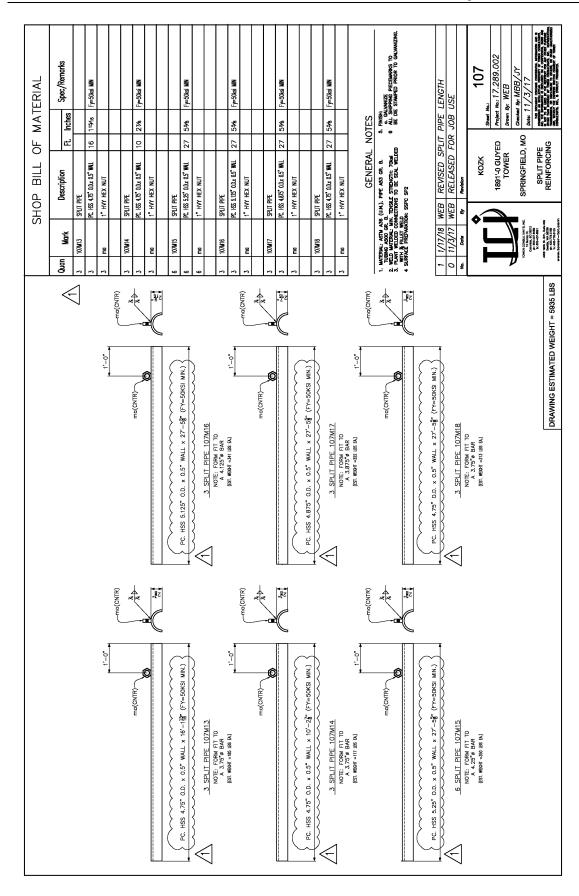


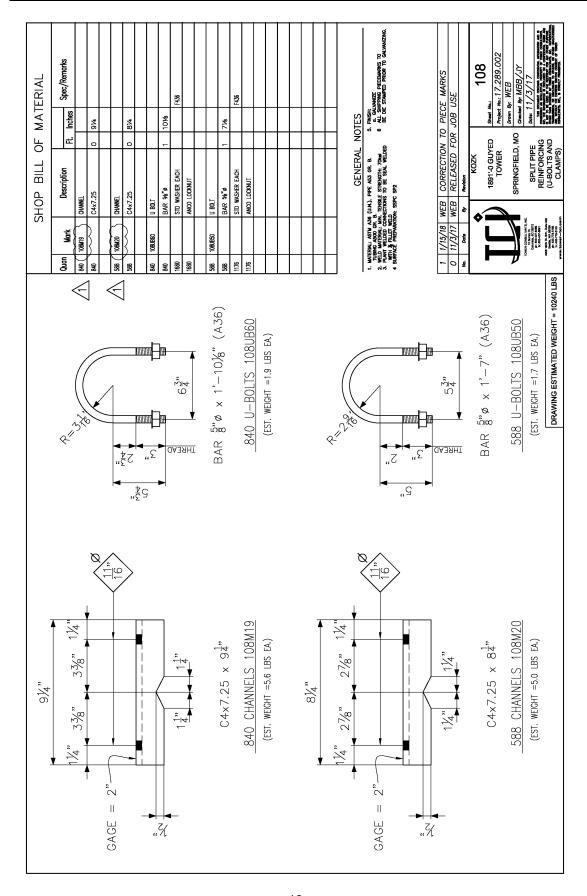


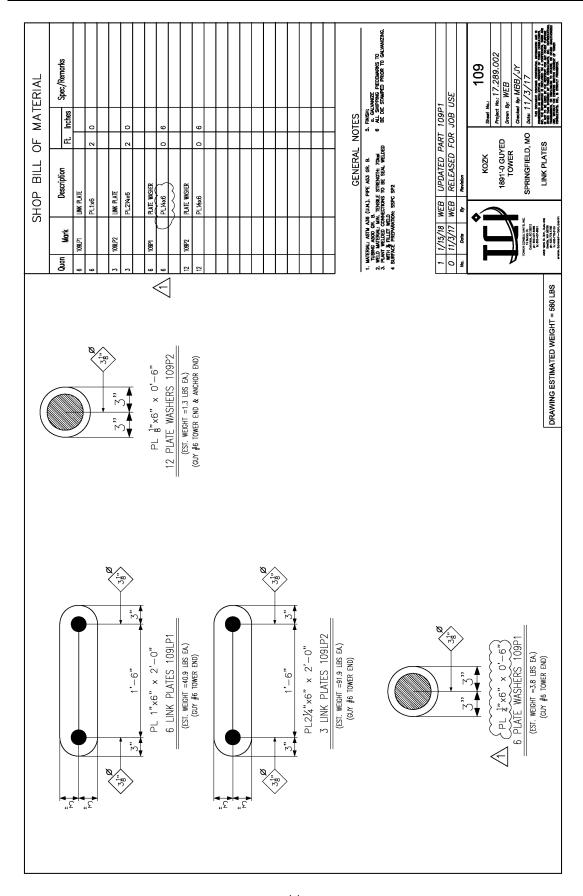


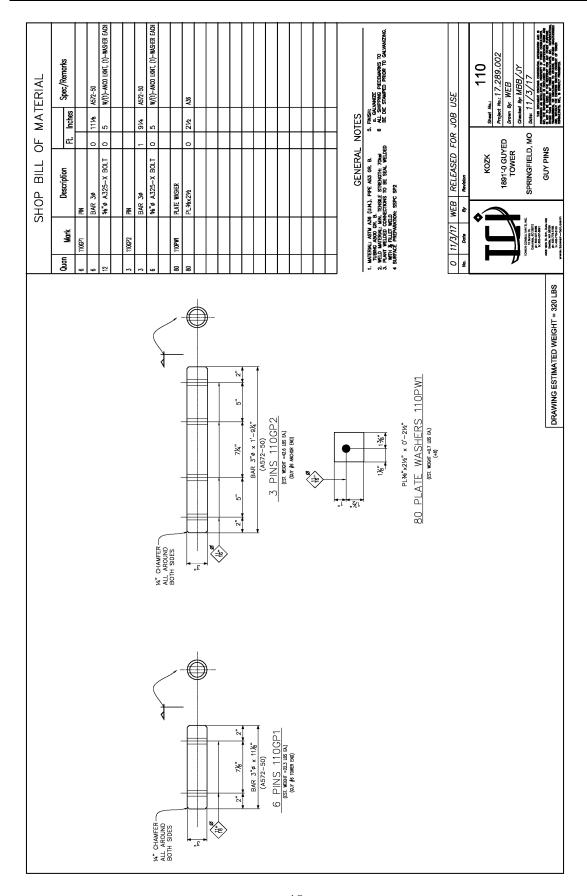


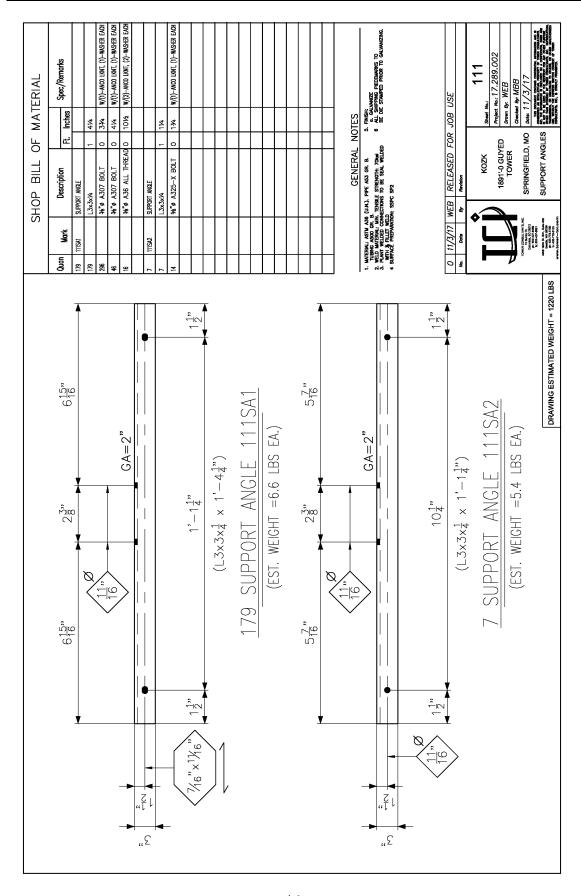


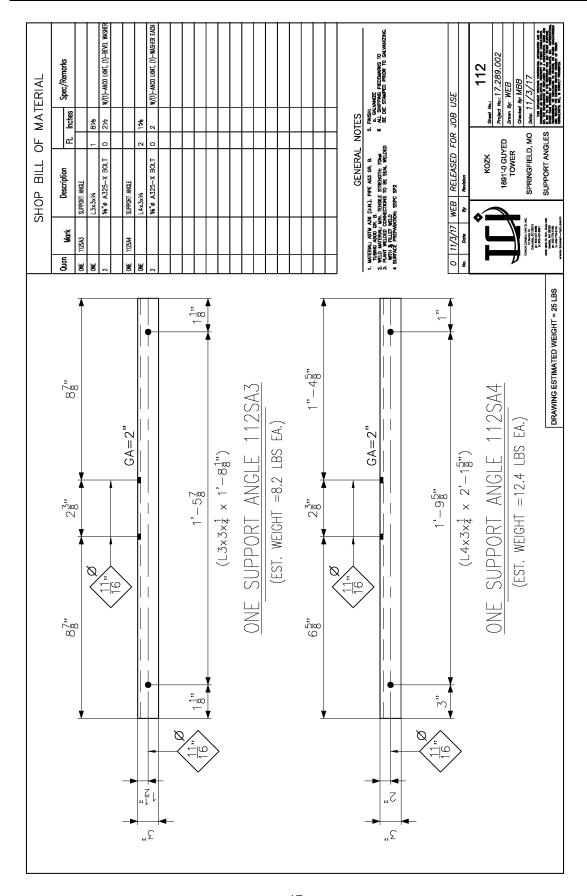


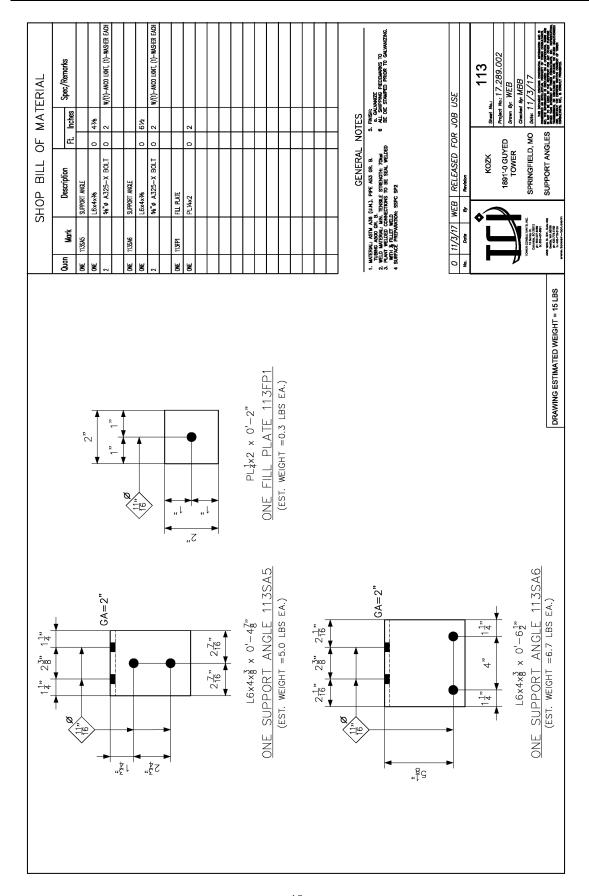


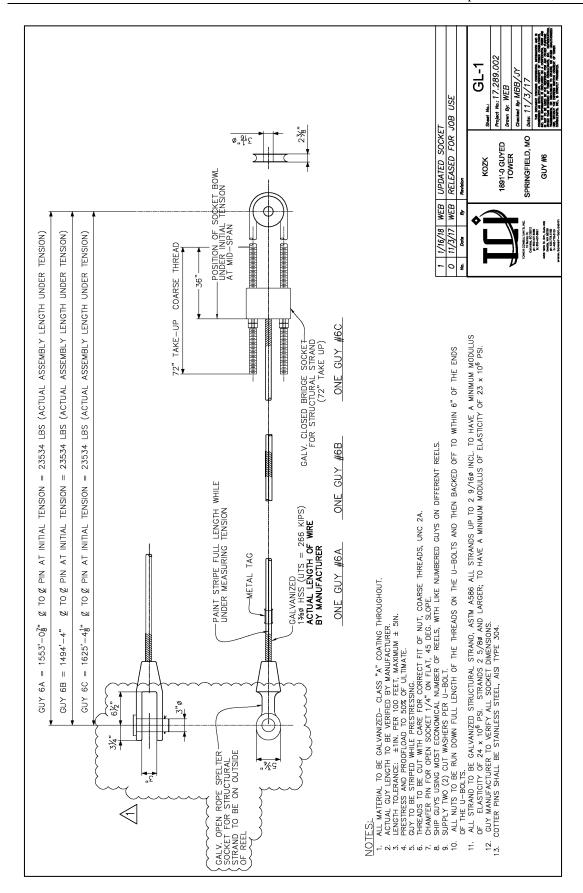












## Appendix C

PHOTOGRAPHS
(APRIL 23, 2018)



Figure C- 1

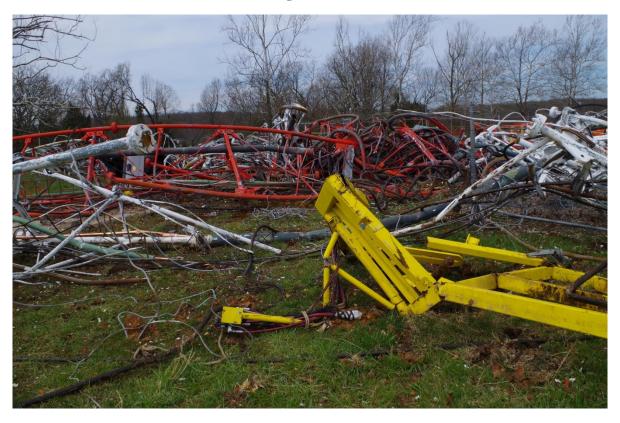


Figure C- 2



Figure C- 3

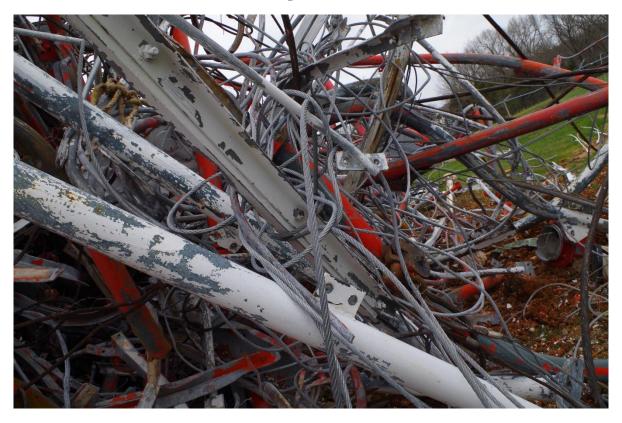


Figure C- 4



Figure C- 5



Figure C- 6



Figure C- 7



Figure C-8



Figure C- 9



Figure C- 10



Figure C- 11

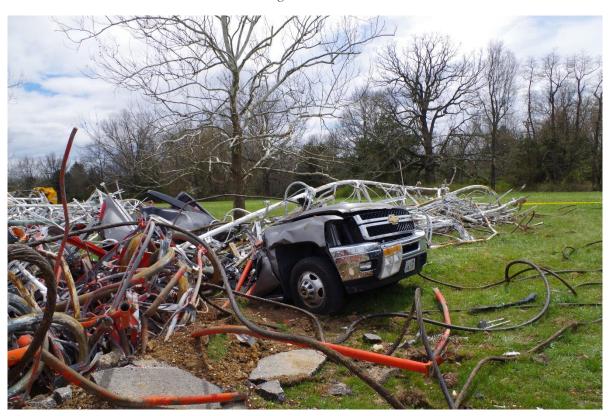


Figure C- 12

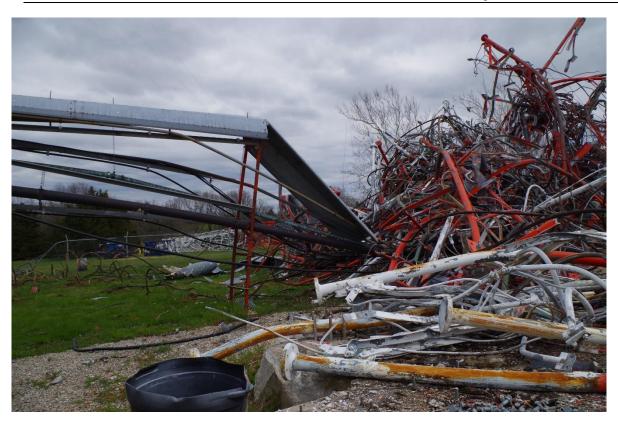


Figure C- 13



Figure C- 14

## Appendix D

PHOTOGRAPHS
(AUGUST 1, 2018)



Figure D- 1



Figure D- 2



Figure D- 3



Figure D- 4



Figure D- 5



Figure D- 6



Figure D- 7



Figure D- 8



Figure D- 9



Figure D- 10

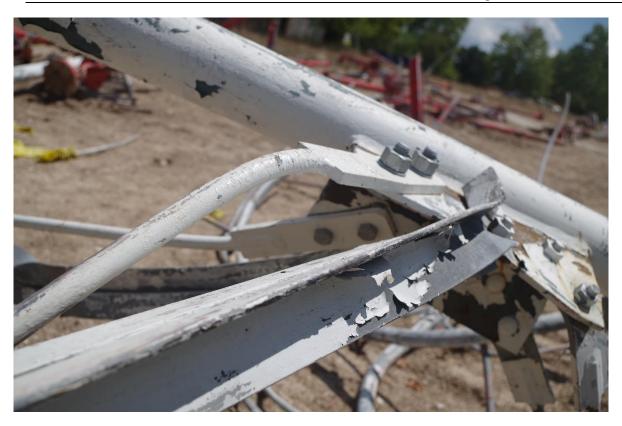


Figure D- 11



Figure D- 12